



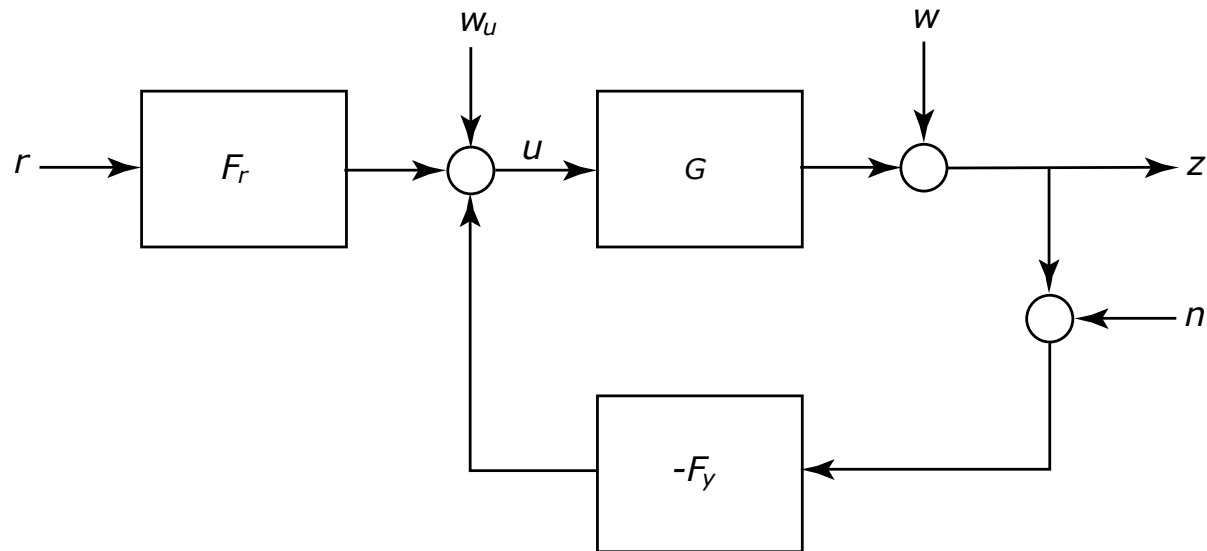
# EL2520

# Control Theory and Practice

## Lecture 3: Robustness

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## So far...



- Signal norms, system gains and the small gain theorem
- The closed-loop system and the design problem
  - Characterized by six transfer functions: need to look at all!
  - Internal stability: stability from all inputs to all outputs (sufficient to check that  $F_r$ ,  $S$ ,  $SG$  and  $SF_y$  are all stable)
  - Sensitivity function (suppression of load disturbances) and Complementary sensitivity (noise, robust stability)

# Goals

After this lecture, you should

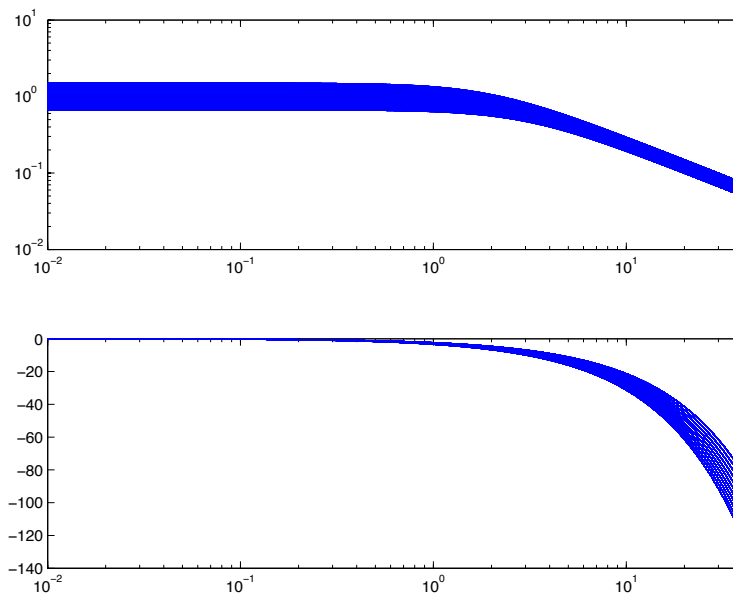
- Understand the concepts of robust stability and robust performance
- Be able to derive multiplicative uncertainty models
  - from parametric uncertainties (e.g. of process pole/zero locations)
  - from frequency responses of multiple plants
- Analyze robust stability using the small-gain theorem
  - “pull out” uncertainty and re-write system on standard form
  - assess robust stability in Bode and Nyquist diagrams

# Motivating example

Assume that you want to control a system on the form

$$G_p(s) = \frac{k}{1 + s\tau} e^{-s\theta}$$

but the values of  $k$ ,  $\tau$ ,  $\theta$  are unknown. You only know that  $k, \tau, \theta \in [2, 3]$



How can we design a controller that is guaranteed to work for all  $G_p$ ?

# Robustness

Robustness=Insensitivity to model errors  
(differences between modelled and actual system behavior)

To reason about uncertainty we need to model it!

- The *uncertainty set*: defines a family of possible models (quantifies how much we do not know about the system)

Would like to establish

- *Robust stability* (stability of all plants in uncertainty set)
- *Robust performance* (meet specs for all plants in uncertainty set)

# Classes of uncertainty

Parametric uncertainty:

- Model structure known, but some parameters are uncertain

Dynamic uncertainty:

- Some (often high frequency) dynamics is missing, either by lack of understanding or in order to get a simpler model

Often, we have a combination of the two.

- Convenient to represent in “lumped” form

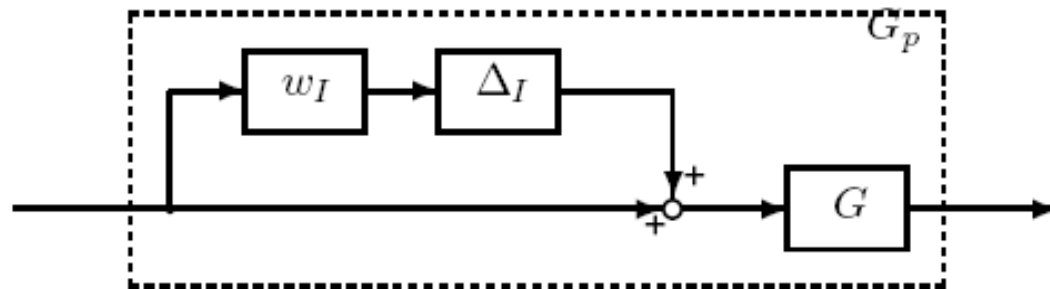
# Multiplicative uncertainty

Multiplicative uncertainty

$$\Pi_I = \{G_p(s) = G(s)(1 + W_I(s)\Delta_I(s)) \mid \|\Delta_I\|_\infty \leq 1\}$$

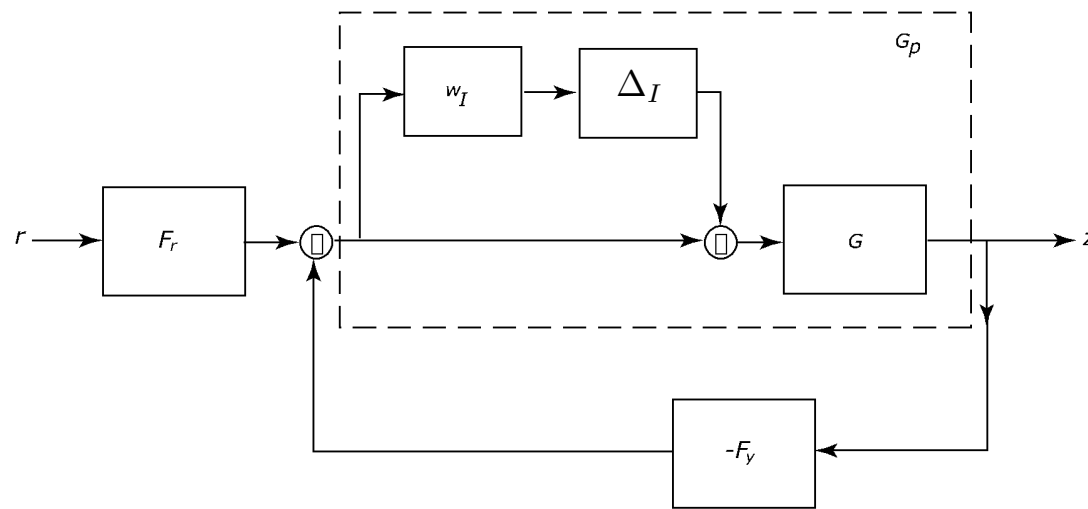
Here,

- $\Pi_I$  is a *family* of possible behaviours of the physical plant
- $\Delta$  is *any* stable transfer function with gain less than one



Robust stability: closed-loop stability for all  $G_p \in \Pi_I$

# Robust stability w. multiplicative uncertainty



Small-gain theorem  $\rightarrow$  interconnection stable if

- (a) nominal closed-loop system is internally stable and  $W_I$  stable, and
- (b)  $\|W_I T\|_\infty \leq 1$

To ensure robust stability:

- first write uncertain system on standard form (find  $G(s)$ ,  $W_I(s)$ )
- make sure that (a) and (b) are satisfied



# Example: uncertain gain

Consider the set of possible plants

$$G_p(s) = kG_0(s), \quad k_{\min} \leq k \leq k_{\max}$$

Any feasible  $k$  can be written as  $k = \bar{k} + r_k \Delta$  for some  $|\Delta| \leq 1$  and

$$\bar{k} = \frac{k_{\min} + k_{\max}}{2}, \quad r_k = \frac{k_{\max} - k_{\min}}{2}$$

Hence, we can re-write the uncertainty in standard form

$$\Pi_I = \left\{ G_p(s) = \underbrace{\bar{k}G_0(s)}_{G(s)} \left( 1 + \underbrace{\frac{r_k}{\bar{k}} \Delta}_{W_I(s)} \right) \mid |\Delta| \leq 1 \right\}$$

Note: here it is enough to let  $\Delta$  be real (in standard form  $\Delta$  is complex)

# Example: uncertain zero location

Consider the set of possible plants

$$G_p(s) = (1 + s\tau)G_0(s), \quad \tau_{\min} \leq \tau \leq \tau_{\max}$$

Can be put into standard form via

$$\bar{\tau} = (\tau_{\min} + \tau_{\max})/2$$

$$r_\tau = (\tau_{\max} - \tau_{\min})/2$$

$$G(s) = (1 + s\bar{\tau})G_0(s)$$

$$W_I(s) = \frac{r_\tau s}{1 + \bar{\tau}s}$$

Note:  $W_I$  is now frequency dependent,  $\Delta$  is still real

# Alternative approach to obtain weight

Note that multiplicative uncertainty class

$$\Pi_I = \{G_p(s) = G(s)(1 + W_I(s)\Delta_I(s)) \mid \|\Delta_I\|_\infty \leq 1\}$$

can be re-written as

$$\Pi_I = \{G_p(s) \mid \|W_I(s)^{-1}G(s)^{-1}(G_p(s) - G(s))\|_\infty \leq 1\}$$

Thus, the uncertainty about the system captured by  $W_I$  if

$$|W_I(i\omega)| \geq \left| \frac{G_p(i\omega) - G(i\omega)}{G(i\omega)} \right| \quad \forall G_p \in \Pi_I, \forall \omega$$

Note: RHS can be interpreted as relative error of nominal model  $G$ .

# Example

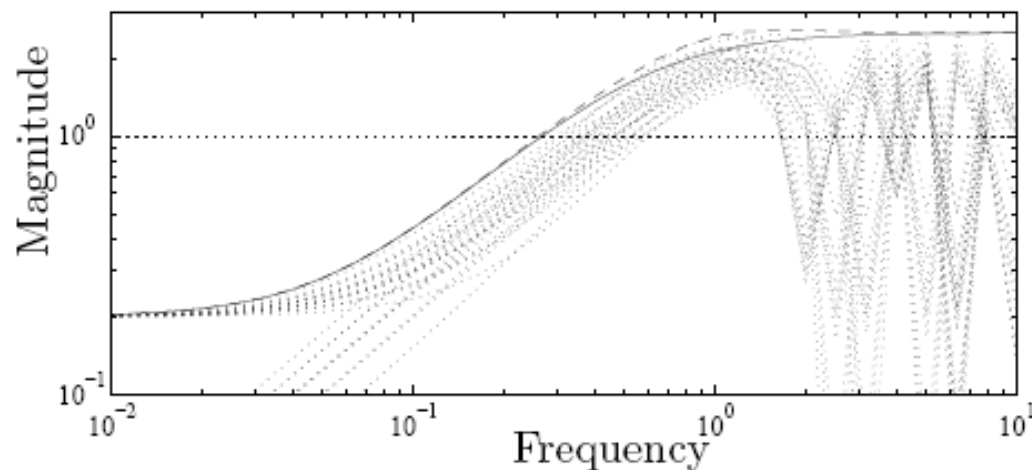
Consider the uncertain system

$$G_p(s) = \frac{k}{\tau s + 1} e^{-\theta s}, \quad k, \theta, \tau \in [2, 3]$$

with nominal plant

$$G(s) = \frac{\bar{k}}{\bar{\tau} s + 1}$$

Sample uncertainties (dotted) and corresponding  $w_I$  (dashed)



# Example: robust stability

Consider the following nominal plant and controller

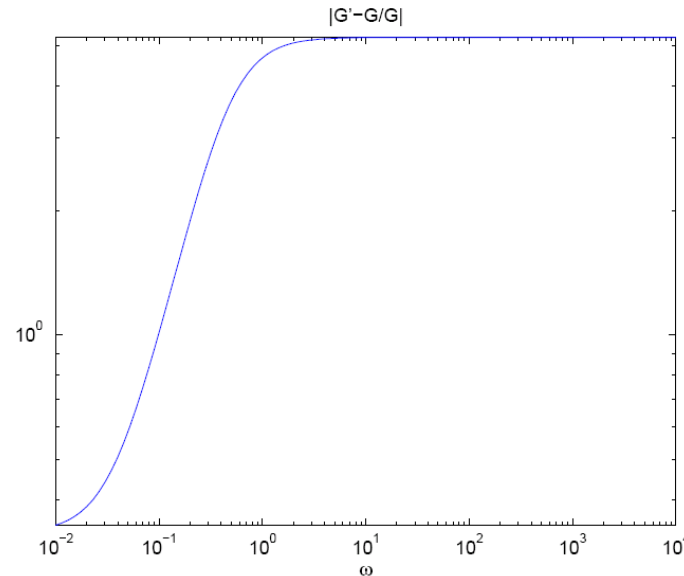
$$G(s) = \frac{3(1 - 2s)}{(5s + 1)(10s + 1)}, \quad K(s) = K_c \frac{12.7s + 1}{12.7s}$$

and assume that one “extreme” possible plant is

$$G'(s) = \frac{4(1 - 3s)}{(4s + 1)^2}$$

# Example: robust stability

Relative error



Is around 0.33 for low frequencies and 5.25 at high frequencies.

Suggests weight

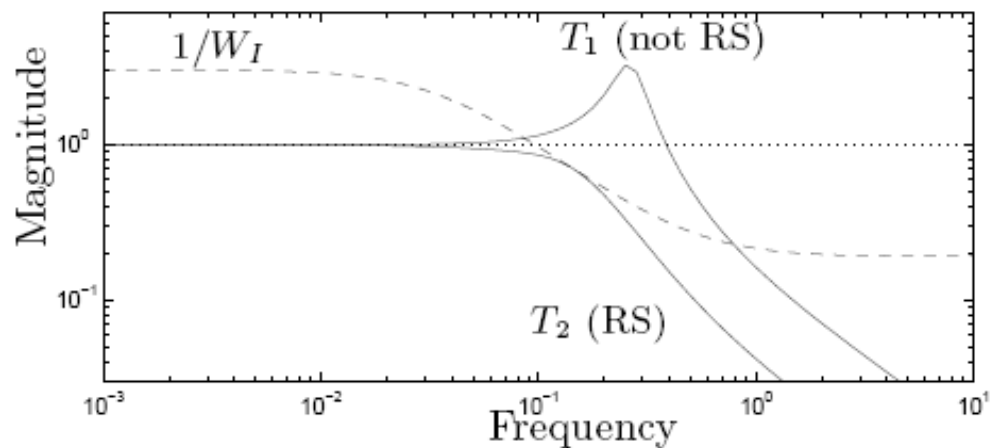
$$W_I(s) = \frac{10s + 0.33}{(10/5.25)s + 1}$$

# Example: robust stability

Robust stability condition  $\|W_I T\|_\infty \leq 1$  holds if  $|T(i\omega)| \leq |W_I^{-1}(i\omega)| \quad \forall \omega$

Hence, we can validate robust stability in the bode diagram of T.

For two controller settings, we obtain two complementary sensitivities

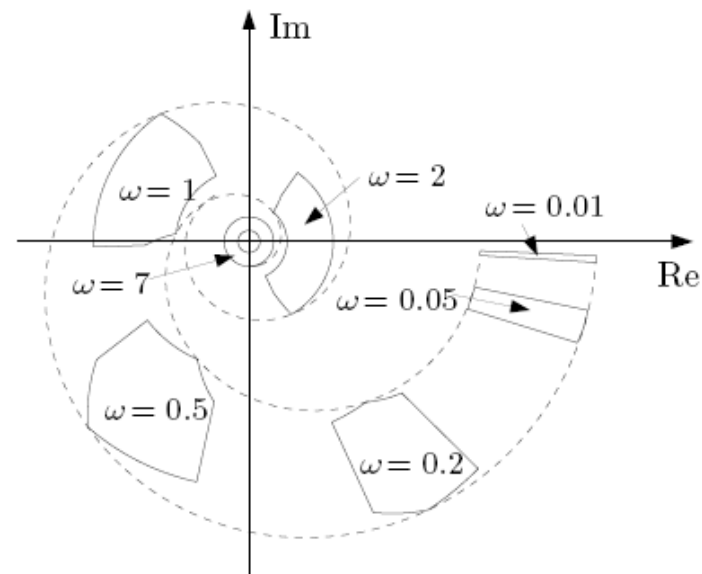


First setting (T1) is not robustly stable, second setting (T2) is.

# Robust stability in the Nyquist curve

Uncertain system:

- $G(i\omega)$  takes one of several possible values at each frequency  
→ a family of Nyquist curves



- Robust stability if uncertainty regions do not encircle -1 point

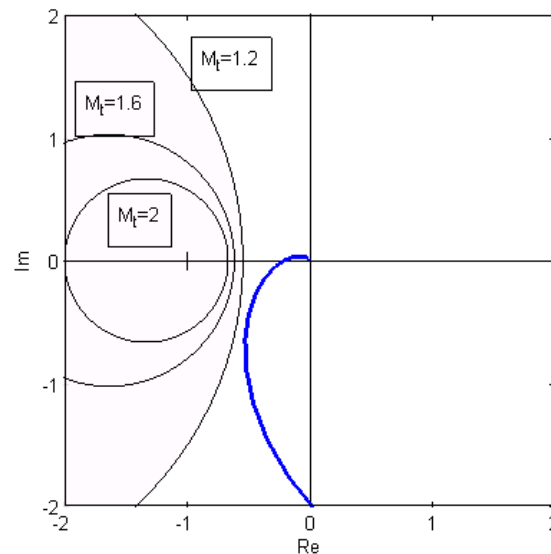


# Complementary sensitivity in Nyquist

Constraint on complementary sensitivity

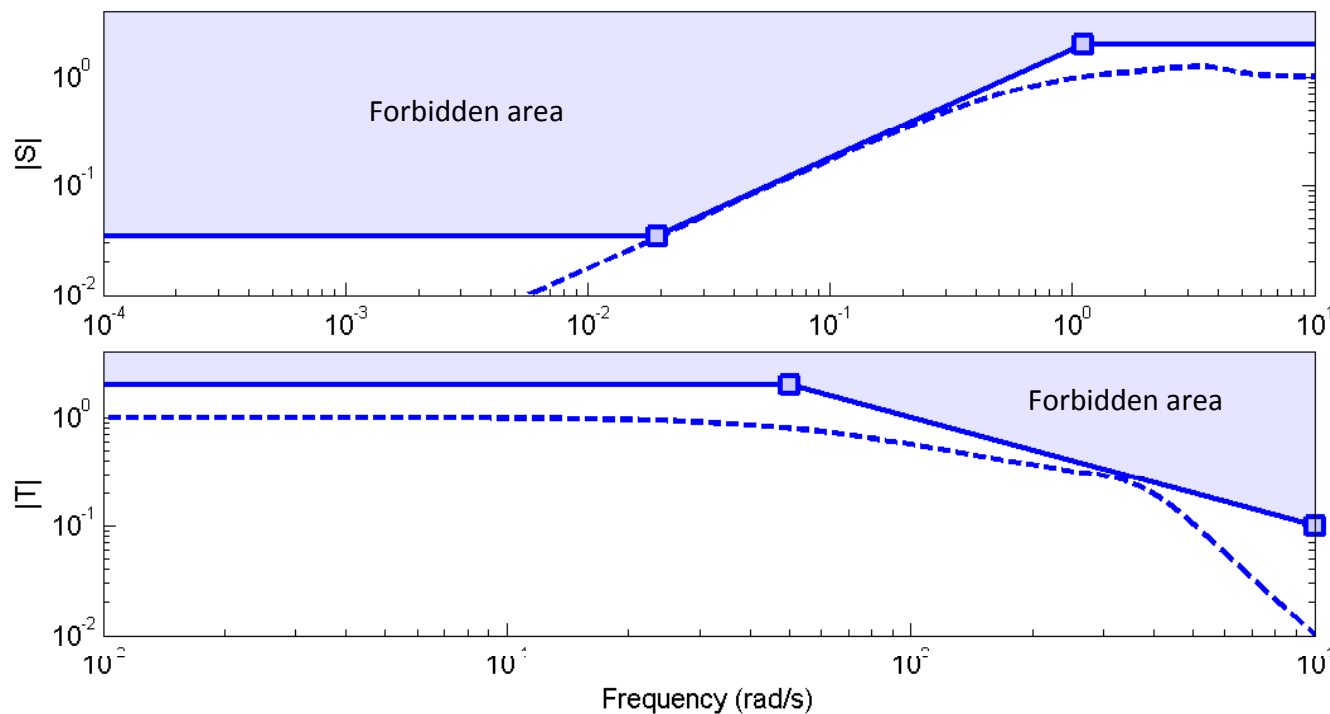
$$\|T(i\omega)\|_{\infty} \leq M_t$$

also yields circles that should be avoided by the Nyquist curve.



Circles centered at  $(-M_t^2/(M_t^2 - 1), 0)$  with radius  $M_t/(M_t^2 - 1)$

# Frequency domain specifications



$$|S(i\omega)| \leq |W_S^{-1}(i\omega)|$$

$$|T(i\omega)| \leq |W_T^{-1}(i\omega)|$$

Can we choose weights  $w_S, w_T$  (“forbidden areas”) freely?

- No, there are many constraints and limitations!

# Extension: shaping the gang of six

Can shape all relevant transfer functions (in “the gang of six”)

$$\|W_S(i\omega)S(i\omega)\|_\infty \leq 1$$

$$\|W_T(i\omega)T(i\omega)\|_\infty \leq 1$$

⋮

$$\|W_{SF_r}(i\omega)S(i\omega)F_r(i\omega)\|_\infty \leq 1$$

This is the topic of Computer Exercise 1b!

# Robust performance

Nominal performance specified in terms of sensitivity function

$$|W_P S| \leq 1 \quad \forall \omega$$

Robust performance

$$|W_P S_p| \leq 1 \quad \text{for all } \omega \text{ and all } S_p$$

Since

$$W_P S_p = W_P \frac{1}{1 + L_p} = \frac{W_P}{1 + L + W_I \Delta L}$$

Worst-case  $\Delta$  is such that  $1+L$  and  $w_I \Delta L$  point in opposite directions

$$|W_P S_p| \leq \frac{|W_P|}{|1 + L| - |W_I L|} = \frac{|W_P S|}{1 - |W_I T|} \quad \forall \omega$$

# Robust performance cont' d

Robust performance

$$|W_P S_p| = \frac{|W_P S|}{1 - |W_I T|} \leq 1$$

Can be expressed as

$$|W_P S| + |W_I T| \leq 1 \quad \forall \omega$$

Sometimes approximated by the *mixed* sensitivity constraint

$$\left\| \begin{pmatrix} W_P S \\ W_I T \end{pmatrix} \right\|_{\infty} \leq 1$$

# Robust stability and performance

In summary

$$\text{nominal performance} \quad |W_P S| \leq 1 \quad \forall \omega$$

$$\text{robust stability} \quad |W_I T| \leq 1 \quad \forall \omega$$

$$\text{robust performance} \quad |W_P S| + |W_I T| \leq 1 \quad \forall \omega$$

Note that nominal performance and robust stability implies

$$|W_P S| + |W_I T| \leq 2 \quad \forall \omega$$

(i.e. robust stability cannot be “too bad”).

Only holds in SISO case.

# Summary

## Robustness

- Insensitivity to model errors

Can guarantee robustness if we model (or bound) uncertainty

- General tool: small gain theorem
- Sometimes need to “pull out” uncertainty by hand
- Sometimes, can fall back onto standard forms (e.g. multiplicative input uncertainty)

Robustness typically introduces new constraints on  $T$

Robust performance: acceptable  $S$ , despite uncertainties.