

## EL2620 Nonlinear Control

### Lecture 11



- Nonlinear controllability
- Gain scheduling

## Today's Goal

You should be able to

- Determine if a nonlinear system is controllable
- Apply gain scheduling to simple examples

## Controllability

### Definition:

$$\dot{x} = f(x, u)$$

is **controllable** if for any  $x^0, x^1$  there exists  $T > 0$  and  $u : [0, T] \rightarrow \mathbb{R}$  such that  $x(0) = x^0$  and  $x(T) = x^1$ .

## Linear Systems

### Lemma:

$$\dot{x} = Ax + Bu$$

is controllable if and only if

$$W_n = (B \quad AB \quad \dots \quad A^{n-1}B)$$

has full rank.

**Is there a corresponding result for nonlinear systems?**

## Controllable Linearization

**Lemma:** Let

$$\dot{z} = Az + Bu$$

be the linearization of

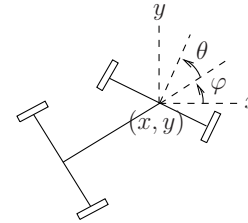
$$\dot{x} = f(x) + g(x)u$$

at  $x = 0$  with  $f(0) = 0$ . If the linear system is controllable then the nonlinear system is controllable in a neighborhood of the origin.

**Remark:**

- Hence, if  $\text{rank } W_n = n$  then there is an  $\epsilon > 0$  such that for every  $x_1 \in B_\epsilon(0)$  there exists  $u : [0, T] \rightarrow \mathbb{R}$  so that  $x(T) = x_1$
- A nonlinear system can be controllable, even if the linearized system is not controllable

## Car Example



Input:  $u_1$  steering wheel velocity,  $u_2$  forward velocity

$$\frac{d}{dt} \begin{pmatrix} x \\ y \\ \varphi \\ \theta \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix} u_1 + \begin{pmatrix} \cos(\varphi + \theta) \\ \sin(\varphi + \theta) \\ \sin(\theta) \\ 0 \end{pmatrix} u_2 = g_1(z)u_1 + g_2(z)u_2$$

Linearization for  $u_1 = u_2 = 0$  gives

$$\dot{z} = Az + B_1 u_1 + B_2 u_2$$

with  $A = 0$  and

$$B_1 = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix}, \quad B_2 = \begin{pmatrix} \cos(\varphi_0 + \theta_0) \\ \sin(\varphi_0 + \theta_0) \\ \sin(\theta_0) \\ 0 \end{pmatrix}$$

$\text{rank } W_n = \text{rank} \begin{pmatrix} B & AB & \dots & A^{n-1}B \end{pmatrix} = 2 < 4$ , so the linearization is not controllable. Still the car is controllable!

**Linearization does not capture the controllability good enough**

## Lie Brackets

Lie bracket between vector fields  $f, g : \mathbb{R}^n \rightarrow \mathbb{R}^n$  is a vector field defined by

$$[f, g] = \frac{\partial g}{\partial x} f - \frac{\partial f}{\partial x} g$$

**Example:**

$$\begin{aligned} f &= \begin{pmatrix} \cos x_2 \\ x_1 \end{pmatrix}, & g &= \begin{pmatrix} x_1 \\ 1 \end{pmatrix} \\ [f, g] &= \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} \begin{pmatrix} \cos x_2 \\ x_1 \end{pmatrix} - \begin{pmatrix} 0 & -\sin x_2 \\ 1 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ 1 \end{pmatrix} \\ &= \begin{pmatrix} \cos x_2 + \sin x_2 \\ -x_1 \end{pmatrix} \end{aligned}$$

## Lie Bracket Direction

For the system

$$\dot{x} = g_1(x)u_1 + g_2(x)u_2$$

the control

$$(u_1, u_2) = \begin{cases} (1, 0), & t \in [0, \epsilon) \\ (0, 1), & t \in [\epsilon, 2\epsilon) \\ (-1, 0), & t \in [2\epsilon, 3\epsilon) \\ (0, -1), & t \in [3\epsilon, 4\epsilon) \end{cases}$$

gives motion

$$x(4\epsilon) = x(0) + \epsilon^2[g_1, g_2] + O(\epsilon^3)$$

**The system can move in the  $[g_1, g_2]$  direction!**

## Proof

1. For  $t \in [0, \epsilon]$ , assuming  $\epsilon$  small and  $x(0) = x_0$ , Taylor series yields

$$x(\epsilon) = x_0 + g_1(x_0)\epsilon + \frac{1}{2} \frac{dg_1}{dx} g_1(x_0)\epsilon^2 + \mathcal{O}(\epsilon^3) \quad (1)$$

2. Similarly, for  $t \in [\epsilon, 2\epsilon]$

$$x(2\epsilon) = x(\epsilon) + g_2(x(\epsilon))\epsilon + \frac{1}{2} \frac{dg_2}{dx} g_2(x(\epsilon))\epsilon^2$$

and with  $x(\epsilon)$  from (1), and  $g_2(x(\epsilon)) = g_2(x_0) + \frac{dg_2}{dx}\epsilon g_1(x_0)$

$$x(2\epsilon) = x_0 + \epsilon(g_1(x_0) + g_2(x_0)) +$$

$$\epsilon^2 \left( \frac{1}{2} \frac{dg_1}{dx}(x_0)g_1(x_0) + \frac{dg_2}{dx}(x_0)g_1(x_0) + \frac{1}{2} \frac{dg_2}{dx}(x_0)g_2(x_0) \right)$$

## Proof, continued

3. Similarly, for  $t \in [2\epsilon, 3\epsilon]$

$$x(3\epsilon) = x_0 + \epsilon g_2 + \epsilon^2 \left( \frac{dg_2}{dx} g_1 - \frac{dg_1}{dx} g_2 + \frac{1}{2} \frac{dg_2}{dx} g_2 \right)$$

4. Finally, for  $t \in [3\epsilon, 4\epsilon]$

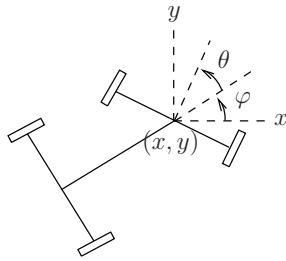
$$x(4\epsilon) = x_0 + \epsilon^2 \left( \frac{dg_2}{dx} g_1 - \frac{dg_1}{dx} g_2 \right)$$

## Car Example (Cont'd)

$$\begin{aligned} g_3 &:= [g_1, g_2] = \frac{\partial g_2}{\partial x} g_1 - \frac{\partial g_1}{\partial x} g_2 \\ &= \begin{pmatrix} 0 & 0 & -\sin(\varphi + \theta) & -\sin(\varphi + \theta) \\ 0 & 0 & \cos(\varphi + \theta) & \cos(\varphi + \theta) \\ 0 & 0 & 0 & \cos(\theta) \\ 0 & 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} 0 \\ 0 \\ 0 \\ 1 \end{pmatrix} - 0 \\ &= \begin{pmatrix} -\sin(\varphi + \theta) \\ \cos(\varphi + \theta) \\ \cos(\theta) \\ 0 \end{pmatrix} \end{aligned}$$

We can hence move the car in the  $g_3$  direction (“wriggle”) by applying the control sequence

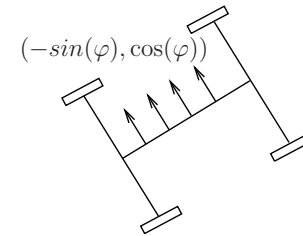
$$(u_1, u_2) = \{(1, 0), (0, 1), (-1, 0), (0, -1)\}$$



The car can also move in the direction

$$g_4 := [g_3, g_2] = \frac{\partial g_2}{\partial x} g_3 - \frac{\partial g_3}{\partial x} g_2 = \dots = \begin{pmatrix} -\sin(\varphi + 2\theta) \\ \cos(\varphi + 2\theta) \\ 0 \\ 0 \end{pmatrix}$$

$g_4$  direction corresponds to sideways movement



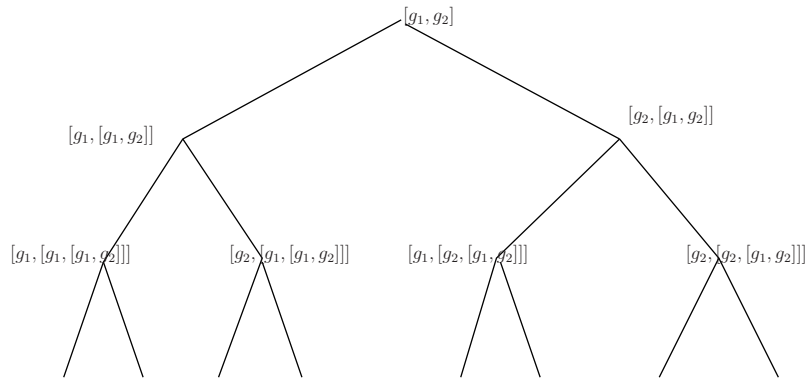
## Parking Theorem

You can get out of any parking lot that is  $\epsilon > 0$  bigger than your car by applying control corresponding to  $g_4$ , that is, by applying the control sequence

Wriggle, Drive, –Wriggle, –Drive

**2 minute exercise:** What does the direction  $[g_1, g_2]$  correspond to for a linear system  $\dot{x} = g_1(x)u_1 + g_2(x)u_2 = B_1u_1 + B_2u_2$ ?

## The Lie Bracket Tree



## Controllability Theorem

**Theorem:** The system

$$\dot{x} = g_1(x)u_1 + g_2(x)u_2$$

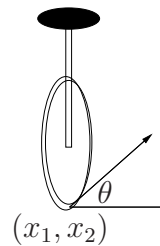
is controllable if the Lie bracket tree (together with  $g_1$  and  $g_2$ ) spans  $\mathbb{R}^n$  for all  $x$

**Remark:**

- The system can be steered in any direction of the Lie bracket tree

## Example—Unicycle

$$\frac{d}{dt} \begin{pmatrix} x_1 \\ x_2 \\ \theta \end{pmatrix} = \begin{pmatrix} \cos \theta \\ \sin \theta \\ 0 \end{pmatrix} u_1 + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} u_2$$



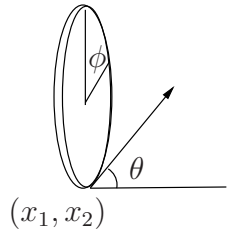
$$g_1 = \begin{pmatrix} \cos \theta \\ \sin \theta \\ 0 \end{pmatrix}, \quad g_2 = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, \quad [g_1, g_2] = \begin{pmatrix} \sin \theta \\ -\cos \theta \\ 0 \end{pmatrix}$$

Controllable because  $\{g_1, g_2, [g_1, g_2]\}$  spans  $\mathbb{R}^3$

**2 minute exercise:**

- Show that  $\{g_1, g_2, [g_1, g_2]\}$  spans  $\mathbb{R}^3$  for the unicycle
- Is the linearization of the unicycle controllable?

### Example—Rolling Penny



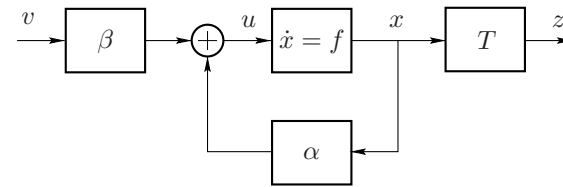
$$\frac{d}{dt} \begin{pmatrix} x_1 \\ x_2 \\ \theta \\ \phi \end{pmatrix} = \begin{pmatrix} \cos \theta \\ \sin \theta \\ 0 \\ 1 \end{pmatrix} u_1 + \begin{pmatrix} 0 \\ 0 \\ 1 \\ 0 \end{pmatrix} u_2$$

Controllable because  $\{g_1, g_2, [g_1, g_2], [g_2, [g_1, g_2]]\}$  spans  $\mathbb{R}^4$

### When is Feedback Linearization Possible?

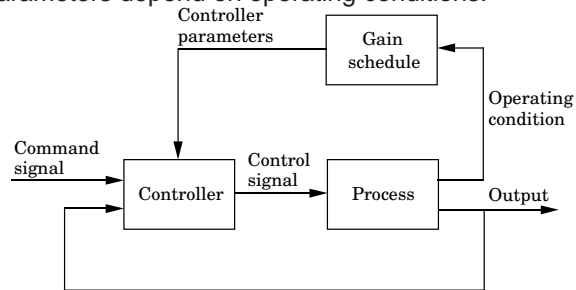
**Q:** When can we transform  $\dot{x} = f(x) + g(x)u$  into  $\dot{z} = Az + bv$  by means of feedback  $u = \alpha(x) + \beta(x)v$  and change of variables  $z = T(x)$  (see previous lecture)?

**A:** The answer requires Lie brackets and further concepts from differential geometry (see Khalil and PhD course)



### Gain Scheduling

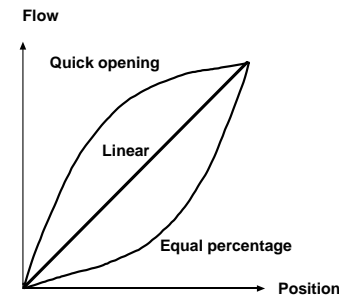
Control parameters depend on operating conditions:



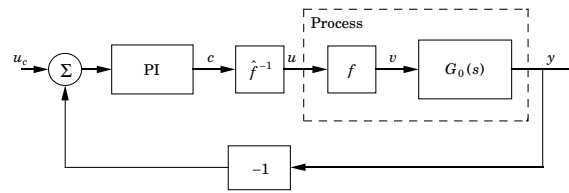
**Example:** PID controller with  $K = K(\alpha)$ , where  $\alpha$  is the scheduling variable.

Examples of scheduling variable are production rate, machine speed, Mach number, flow rate

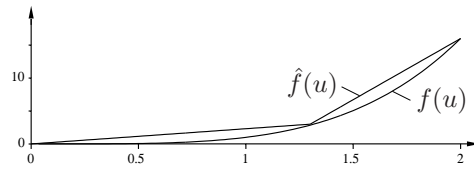
### Valve Characteristics



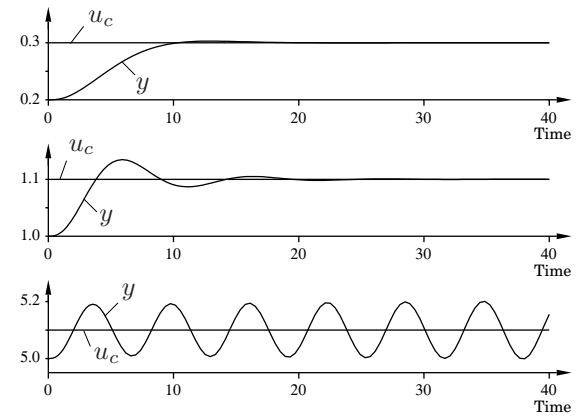
## Nonlinear Valve



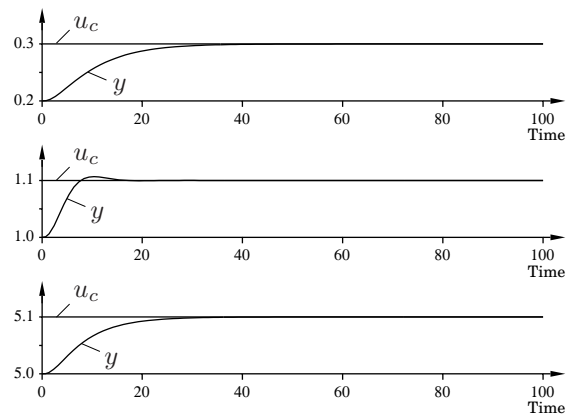
Valve characteristics



Without gain scheduling:

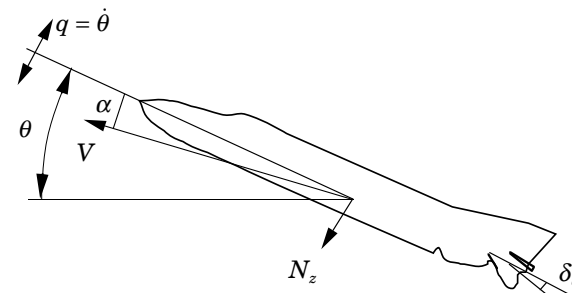


With gain scheduling:



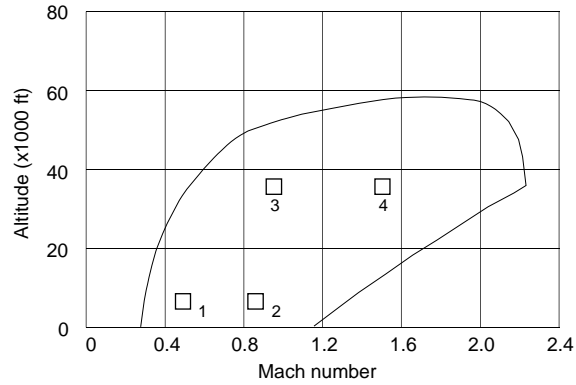
## Flight Control

Pitch dynamics

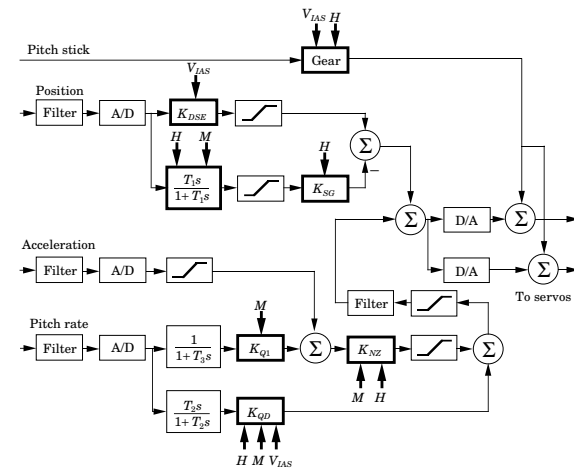


## Flight Control

Operating conditions:



## The Pitch Control Channel



## Today's Goal

You should be able to

- Determine if a nonlinear system is controllable
- Apply gain scheduling to simple examples

## Next Lecture

- Optimal control