• Disposition

Instructors

7.5 credits, *lp* 2

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#### **Course Goal**

To provide participants with a solid theoretical foundation of nonlinear control systems combined with a good engineering understanding

You should after the course be able to

- understand common nonlinear control phenomena
- apply the most powerful nonlinear analysis methods
- use some practical nonlinear control design methods

Mathematically describe common nonlinearities in control

• Transform differential equations to first-order form

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 EL2620 Nonlinear Control
 Today's Goal

 Lecture 1
 You should be able to

 • Describe distinctive phenomena in nonlinear dynamic systems

(KTH)

- Practical information
- Course outline
- Linear vs Nonlinear Systems
- Nonlinear differential equations

EL2620 Nonlinear Control Automatic Control Lab, KTH

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STEX (entrance floor, Osquldasv. 10), course material

28h lectures, 28h exercises, 3 home-works

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systems

Derive equilibrium points

#### Material

- Textbook: Khalil, Nonlinear Systems, Prentice Hall, 3rd ed., 2002. Optional but highly recommended.
- Lecture notes: Copies of transparencies (from previous year)
- Exercises: Class room and home exercises
- Homeworks: 3 computer exercises to hand in (and review)
- Software: Matlab

Alternative textbooks (decreasing mathematical brilliance): Sastry, Nonlinear Systems: Analysis, Stability and Control; Vidyasagar, Nonlinear Systems Analysis; Slotine & Li, Applied Nonlinear Control; Glad & Ljung, Reglerteori, flervariabla och olinjära metoder. Only references to Khalil will be given.

Two course compendia sold by STEX.

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#### **Course Outline**

**Course Information** 

http://www.ee.kth.se/control/courses/EL2620

• Homeworks are compulsory and have to be handed in on time

• Everyone will receive the homework of another student for review

All info and handouts are available at

(compulsory).

- Introduction: nonlinear models and phenomena, computer simulation (L1-L2)
- Feedback analysis: linearization, stability theory, describing functions (L3-L6)
- Control design: compensation, high-gain design, Lyapunov methods (L7-L10)
- Alternatives: gain scheduling, optimal control, neural networks, fuzzy control (L11-L13)
- Summary (L14)

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#### **Linear Systems**

**Definition:** Let M be a signal space. The system  $S: M \to M$  is linear if for all  $u, v \in M$  and  $\alpha \in \mathbb{R}$ 

$$S(\alpha u) = \alpha S(u)$$
 scaling  
 $S(u+v) = S(u) + S(v)$  superposition

#### **Example:** Linear time-invariant systems

$$\dot{x}(t) = Ax(t) + Bu(t), \quad y(t) = Cx(t), \quad x(0) = 0$$
$$y(t) = g(t) \star u(t) = \int_0^t g(\tau)u(t-\tau)d\tau$$
$$Y(s) = G(s)U(s)$$

Notice the importance to have zero initial conditions

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# Linear Models may be too Crude Approximations

Example: Positioning of a ball on a beam





Nonlinear model:  $m\ddot{x}(t) = mg\sin\phi(t)$ , Linear model:  $\ddot{x}(t) = g\phi(t)$ 

Linear Models are not Rich Enough

Linear models can not describe many phenomena seen in nonlinear systems



Can the ball move 0.1 meter in 0.1 seconds from steady state?

**Linear Systems Have Nice Properties** 

Local stability=global stability Stability if all eigenvalues of A (or

Superposition Enough to know a step (or impulse) response

Frequency analysis possible Sinusoidal inputs give sinusoidal

poles of G(s)) are in the left half-plane

outputs:  $Y(i\omega) = G(i\omega)U(i\omega)$ 

Linear model (step response with  $\phi = \phi_0$ ) gives

$$x(t) \approx 10 \frac{t^2}{2} \phi_0 \approx 0.05 \phi_0$$

so that

$$\phi_0 \approx \frac{0.1}{0.05} = 2 \text{ rad} = 114^\circ$$

#### Unrealistic answer. Clearly outside linear region!

Linear model valid only if  $\sin \phi \approx \phi$ 

Must consider nonlinear model. Possibly also include other nonlinearities such as centripetal force, saturation, friction etc.

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# Stability Can Depend on Reference Signal

**Example:** Control system with valve characteristic  $f(u) = u^2$ 



Simulink block diagram:



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# **Multiple Equilibria**

Example: chemical reactor



Existence of multiple stable equilibria for the same input gives hysteresis effect





#### Stability depends on amplitude of the reference signal!

(The linearized gain of the valve increases with increasing amplitude)



## **Stable Periodic Solutions**

Example: Position control of motor with back-lash



Motor:  $G(s) = \frac{1}{s(1+5s)}$ Controller: K = 5 2010

#### Back-lash induces an oscillation

Period and amplitude independent of initial conditions:



#### How predict and avoid oscillations?

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## **Harmonic Distortion**

Example: Sinusoidal response of saturation



## **Automatic Tuning of PID Controllers**

Relay induces a desired oscillation whose frequency and amplitude are used to choose PID parameters



#### **Example:** Electrical power distribution

Nonlinearities such as rectifiers, switched electronics, and transformers give rise to harmonic distortion

Total Harmonic Distortion = 
$$\frac{\sum_{k=2}^{\infty} \text{Energy in tone } k}{\text{Energy in tone 1}}$$

#### **Example:** Electrical amplifiers

Effective amplifiers work in nonlinear region

Introduces spectrum leakage, which is a problem in cellular systems Trade-off between effectivity and linearity

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## **Subharmonics**

**Example:** Duffing's equation  $\ddot{y} + \dot{y} + y - y^3 = a \sin(\omega t)$ 



## **Nonlinear Differential Equations**

Definition: A solution to

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$$\dot{x}(t) = f(x(t)), \quad x(0) = x_0$$
 (1)

over an interval [0,T] is a  ${\bf C}^1$  function  $x:[0,T]\to \mathbb{R}^n$  such that (1) is fulfilled.

- When does there exists a solution?
- When is the solution unique?

**Example:**  $\dot{x} = Ax$ ,  $x(0) = x_0$ , gives  $x(t) = \exp(At)x_0$ 

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## Finite Escape Time

Simulation for various initial conditions  $x_0$ 



## **Existence Problems**

**Example:** The differential equation  $\dot{x} = x^2$ ,  $x(0) = x_0$ 

has solution 
$$x(t) = \frac{x_0}{1 - x_0 t}, \qquad 0 \le t < \frac{1}{x_0}$$

Solution not defined for 
$$t_f =$$

Solution interval depends on initial condition!

 $\frac{1}{x_0}$ 

Recall the trick: 
$$\dot{x} = x^2 \Rightarrow \frac{dx}{x^2} = dt$$
  
Integrate  $\Rightarrow \frac{-1}{x(t)} - \frac{-1}{x(0)} = t \Rightarrow x(t) = \frac{x_0}{1 - x_0 t}$ 

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## **Uniqueness Problems**



# $x(t) = \begin{cases} (t - C)^2/4 & t > C \\ 0 & t \le C \end{cases}$



2 Time t

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# **Lipschitz Continuity**

**Definition:**  $f : \mathbb{R}^n \to \mathbb{R}^n$  is Lipschitz continuous if there exists L, r > 0 such that for all  $x, y \in B_r(x_0) = \{ z \in \mathbb{R}^n : ||z - x_0|| < r \},\$ 



Euclidean norm is given by

$$||x||^2 = x_1^2 + \dots + x_n^2$$



# **Physical Interpretation**

Consider the reverse example, i.e., the water tank lab process with

 $\dot{x} = -\sqrt{x}, \qquad x(T) = 0$ 

where x is the water level. It is then impossible to know at what time t < T the level was  $x(t) = x_0 > 0$ .

*Hint:* Reverse time  $s = T - t \Rightarrow ds = -dt$  and thus

$$\frac{dx}{ds} = -\frac{dx}{dt}$$

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## Local Existence and Uniqueness

#### Theorem:

If f is Lipschitz continuous, then there exists  $\delta > 0$  such that

$$\dot{x}(t) = f(x(t)), \qquad x(0) = x_0$$

has a unique solution in  $B_r(x_0)$  over  $[0, \delta]$ . **Proof:** See Khalil, Appendix C.1. Based on the contraction mapping theorem

#### Remarks

- $\delta = \delta(r, L)$
- f being  $C^0$  is not sufficient (cf., tank example)
- f being  $C^1$  implies Lipschitz continuity  $(L = \max_{x \in B_r(x_0)} f'(x))$

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# **State-Space Models**

State x, input u, output y

General:

 $\dot{x} = f(x, u), \quad y = h(x)$ Explicit:

 $\dot{x} = f(x) + q(x)u, \quad y = h(x)$ Affine in *u*:

Linear:  $\dot{x} = Ax + Bu, \quad y = Cx$ 

 $f(x, u, y, \dot{x}, \dot{u}, \dot{y}, \ldots) = 0$ 

## **Transformation to Autonomous System**

A nonautonomous system

 $\dot{x} = f(x,t)$ 

is always possible to transform to an autonomous system by introducing  $x_{n+1} = t$ :

$$\dot{x} = f(x, x_{n+1})$$
$$\dot{x}_{n+1} = 1$$

## **Transformation to First-Order System**

Given a differential equation in y with highest derivative  $\frac{d^n y}{dt^n}$ , express the equation in  $x = \begin{pmatrix} y & \frac{dy}{dt} & \dots & \frac{d^{n-1}y}{dt^{n-1}} \end{pmatrix}^T$  Example:

Pendulum

$$MR^2\ddot{\theta} + k\dot{\theta} + MgR\sin\theta = 0$$

 $x = (\theta \ \theta)^{T}$  gives

$$\dot{x}_1 = x_2$$
$$\dot{x}_2 = -\frac{k}{MR^2}x_2 - \frac{g}{R}\sin x_1$$

**Equilibria** 

**Definition:** A point  $(x^*, u^*, y^*)$  is an equilibrium, if a solution starting in  $(x^*, u^*, y^*)$  stays there forever.

Corresponds to putting all derivatives to zero:

General:	$f(x^*, u^*, y^*, 0, 0, \ldots) = 0$
Explicit:	$0 = f(x^*, u^*),  y^* = h(x^*)$
Affine in u:	$0=f(x^*)+g(x^*)u^*,  y^*=h(x^*)$
Linear:	$0 = Ax^* + Bu^*,  y^* = Cx^*$

Often the equilibrium is defined only through the state  $x^*$ 

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#### Some Common Nonlinearities in Control **Multiple Equilibria Systems** Example: Pendulum e<sup>u</sup> |u| $MR^2\ddot{\theta} + k\dot{\theta} + MqR\sin\theta = 0$ Abs Math Saturation $\ddot{\theta} = \dot{\theta} = 0$ gives $\sin \theta = 0$ and thus $\theta^* = k\pi$ Function Alternatively in first-order form: \_ook\_Ur Dead Zone Sign Table $\dot{x}_1 = x_2$ $\dot{x}_2 = -\frac{k}{MB^2}x_2 - \frac{g}{B}\sin x_1$ $\dot{x}_1 = \dot{x}_2 = 0$ gives $x_2^* = 0$ and $\sin(x_1^*) = 0$ Relay Backlash Coulomb & Viscous Friction 33 34 Lecture 1 Lecture 1 EL2620 2010 EL2620 2010 When do we need Nonlinear Analysis & **Design? Next Lecture** • When the system is strongly nonlinear Simulation in Matlab • When the range of operation is large Linearization • When distinctive nonlinear phenomena are relevant • Phase plane analysis • When we want to push performance to the limit

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