



Parameter estimation: a key ingredient for the application of sonAIR

Olivier Schwab (olivier.schwab@empa.ch)

Empa, Laboratory for Acoustics / Noise Control

Abteilungsbesuch Direktion — January 28, 2018

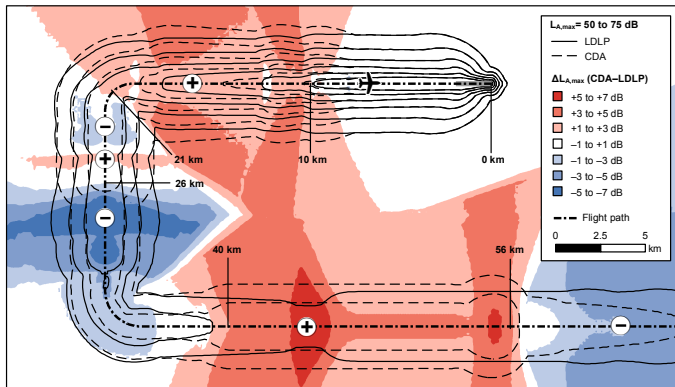
- 1 **Introduction:** a quick recap on sonAIR
- 2 **Motivation:** the need for a parameter estimation
- 3 **Methods:**
 - ▶ the machine learning solution for the aerodynamic part
 - ▶ the engineering solution for the engine part
- 4 **Summary:** increased accuracy
- 5 **Challenges and next steps:** towards generalization
- 6 **Outlook:** live aircraft noise calculations with sonAIR

Introduction: a quick recap on sonAIR

An emission model for the accurate simulation of single flights

- The emission model accounts for both engine and airframe noise
- Considers the most important effects based on physics
 - ▶ Directivity (θ, φ)
 - ▶ Engine power ($N1, N1^2$)
 - ▶ Aeroacoustic sources (Ma, ρ)
 - ▶ Configuration (LG, FH, SB)
 - ▶ Interactions (e.g. change of directivity with engine power)
- Spectral model in 1/3 octave bands, between 25 Hz – 5 kHz

- Increased accuracy for standard applications
 - ▶ Calculation of noise maps for yearly traffic
- Unique new applications
 - ▶ Assessment and optimization of noise abatement procedures



Motivation: the need for a parameter estimation

Engine and airframe input parameters are needed

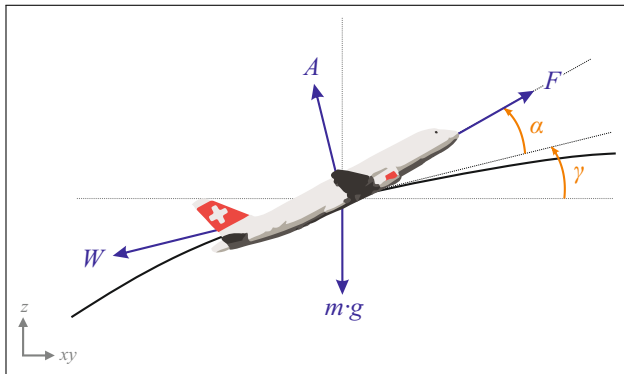
- Commonly available inputs:
 - ▶ Radar data: $x(t), y(t), z(t)$
 - ▶ List of movements: aircraft type, date, time, [mass], destination, ...
- Required sonAIR inputs:
 - ▶ Directivity (θ, φ) → from geometry ✓
 - ▶ Engine power ($N1, N1^2$) → ✗
 - ▶ Aeroacoustic sources (Ma, ρ) → from geometry and ISA ✓
 - ▶ Configuration (LG, FH, SB) → ✗

→ For the application of sonAIR, it is essential to determine the missing engine and airframe parameters: **$N1$** and **configuration**

Is a solution by calculation possible?

Problem: estimate $N1$ ($\leftarrow F$), flap handle ($\leftarrow A$), landing gear ($\leftarrow W$)

$$\begin{cases} m \cdot a_{xy} &= F \cdot \cos(\gamma + \alpha) - W \cdot \cos \gamma + A \cdot \cos\left(\frac{\pi}{2} + \gamma\right) \\ m \cdot a_z &= F \cdot \sin(\gamma + \alpha) - W \cdot \sin \gamma + A \cdot \sin\left(\frac{\pi}{2} + \gamma\right) - m \cdot g \end{cases}$$



Separation into two independent sub-problems

- From balance of forces:
 - ▶ Too many unknowns for direct solution
 - ▶ No unique solution for configuration (e.g. Δ in lift caused by flap change can be compensated for by angle-of-attack)
- The problem is divided into two independent problems
 - ① The configuration is estimated using machine learning
 - ② $N1$ is estimated using an engineering approach
- Assumptions for independence of the two sub-problems:
 - ▶ Configuration changes occur mainly based on altitude / aircraft speed
 - ▶ $N1$ estimation assumes a mean configuration profile
- Restriction: requires training data

→ shown here: ① for approaches, ② for departures

Methods: the machine learning solution for the aerodynamic part

Configuration is a machine learning problem

- Configuration cannot be solved for uniquely, but for each point in time there is a most likely configuration
- Machine learning problem: classification task with supervised learning:

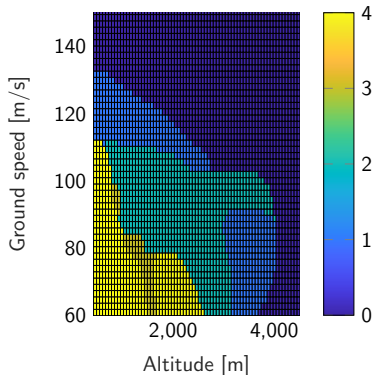
$$\{h, v, v_z\} \rightarrow \{\text{flap handle, landing gear}\}$$

- Possible to build for approaches and departures for all available aircraft types
- Example here: SVM classifier
→ hyperplane so that the distance from it to the nearest data point on each side is maximized

Example: classifiers for approaches A320

① Flap handle:

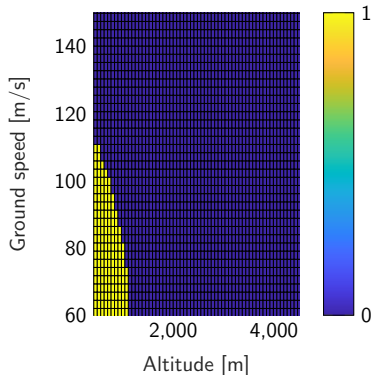
$$\{h, v\} \rightarrow \{\text{flap handle}\}$$



Estimated accuracy: 82%
(cross-validation)

② Landing gear:

$$\{h, v\} \rightarrow \{\text{landing gear}\}$$

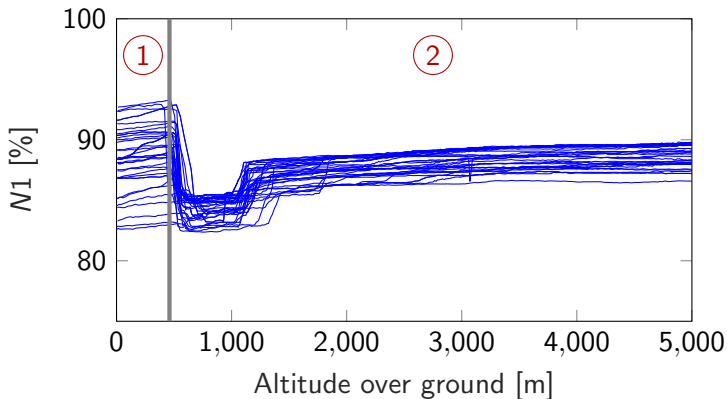


Estimated accuracy: 96%
(cross-validation)

Methods: the engineering solution for the engine part

Departures are modeled by segment-wise $N1$ -profiles

$N1$ -profiles A320



Segment-wise $N1$ -profiles: ① flex take-off ② de-rated climb

Take-off profiles account for flex take-off

Ansatz:
$$N1_{h=h_i}^2 = a_0 + a_1 \cdot m \cdot \cos \bar{\gamma} + a_2 \cdot m \cdot \sin \bar{\gamma} + a_3 \cdot T_{h=h_i}$$

- Thrust is a function of mass and climb behavior (balance of forces under assumptions $a \approx 0$, $\gamma \approx \text{const.} = \bar{\gamma}$):

$$F = f(m \cdot \cos \bar{\gamma}, m \cdot \sin \bar{\gamma})$$

- Thrust is a quadratic function of $N1$:

$$F_{h=h_i} \propto N1_{h=h_i}^2$$

- $N1^2$ is approximately linearly dependent on temperature:

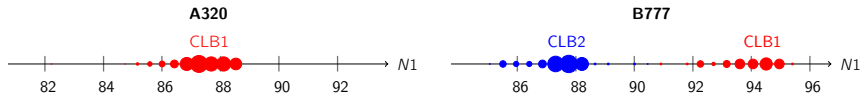
$$N1_{h=h_i}^2 \propto T_{h=h_i}$$

- [Proxy for aircraft mass: $m \propto v_{IC}^2$]

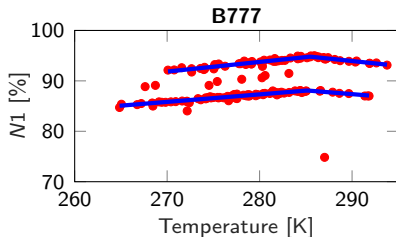
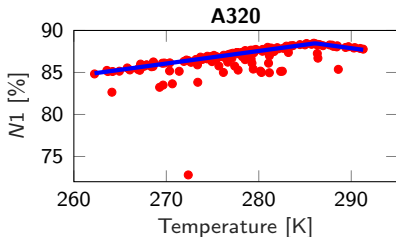
Climb profiles account for de-rated climb

Ansatz: ① per de-rate ② $N1_{h=h_i} = a \cdot |T_{h=h_i} - b| + c$

- One or two de-rated climb settings, e.g. N1 at $h = 2000$ m over ground



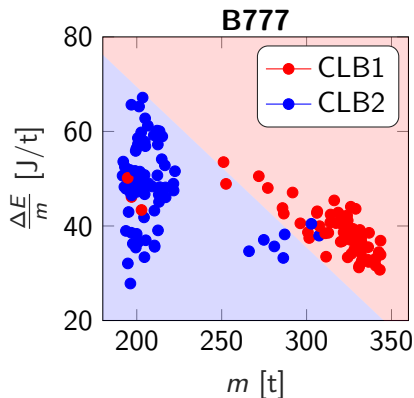
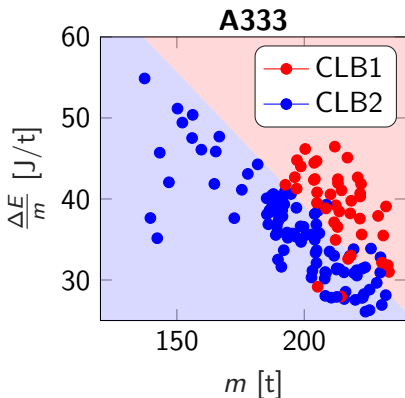
- Variance inside climb setting is due to temperature variations



How to distinguish climb settings?

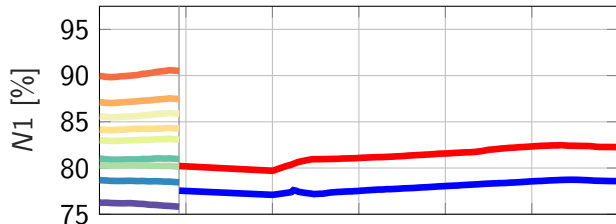
Two factors to consider: aircraft mass m and increase in energy ΔE between two points in time t_1 and t_2 , e.g. $h_1 = h(t_1) = 1\,000$ m over ground and $h_2 = h(t_2) = h(t_1 + 300 \text{ s})$.

$$\textcircled{1} \quad m \quad \textcircled{2} \quad \frac{\Delta E}{m} = 0.5 \cdot (v_2^2 - v_1^2) + g \cdot (h_2 - h_1)$$



Example $N1$ -profiles for A333

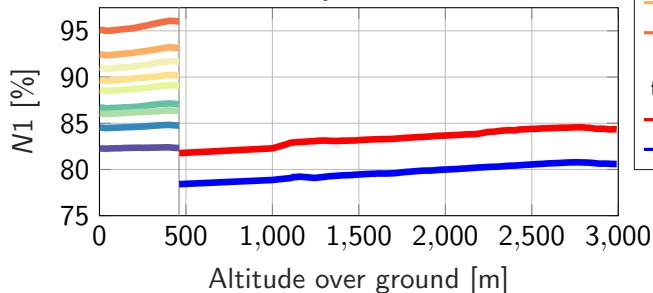
Ground temperature $T=0^{\circ}\text{C}$



close range:

- $m = 170 \text{ t}, \bar{\gamma} = 8^{\circ}$
- $m = 170 \text{ t}, \bar{\gamma} = 10^{\circ}$
- $m = 170 \text{ t}, \bar{\gamma} = 12^{\circ}$
- $m = 200 \text{ t}, \bar{\gamma} = 8^{\circ}$
- $m = 200 \text{ t}, \bar{\gamma} = 10^{\circ}$
- $m = 200 \text{ t}, \bar{\gamma} = 12^{\circ}$
- $m = 230 \text{ t}, \bar{\gamma} = 8^{\circ}$
- $m = 230 \text{ t}, \bar{\gamma} = 10^{\circ}$
- $m = 230 \text{ t}, \bar{\gamma} = 12^{\circ}$

Ground temperature $T=30^{\circ}\text{C}$



far range: CLB

- CLB1
- CLB2

Summary: increased accuracy

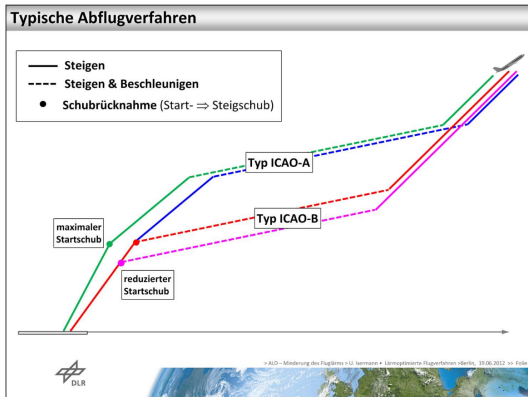
Roundup and conclusions

- sonAIR is able to provide increased accuracy for existing aircraft noise applications as well as the application to new kinds of investigations using single flights
- The parameter estimation is crucial for the application of sonAIR
- The solution consists in
 - ▶ Using machine learning for the configuration problem
 - ▶ Using an engineering approach for the $N1$ estimation problem
- Validation shows good agreement, resulting in receiver L_{AE} errors of less than 1 dB for both close and far range
- Solution works for non-SWISS aircraft and other airports

Challenges and next steps: towards generalization

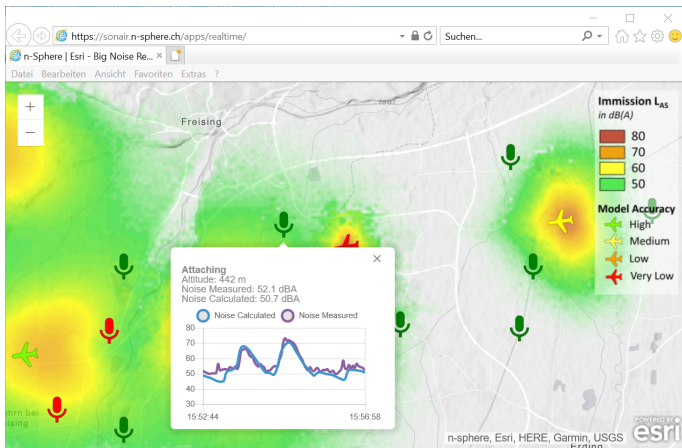
Improvements for further generalization

- Addition of new aircraft types, e.g. Bombardier C-Series
- Improve training database for non-SWISS aircraft
 - ▶ In-house *N1* determination from acoustics
- Investigation into procedures for a variation of airlines and airports
 - ▶ ICAO Noise Abatement Departure Procedures NADP 1&2:



Outlook: live aircraft noise calculations with sonAIR

Pilot project for Airbus: Empa in cooperation with partner n-Sphere



Thank you for your attention. Questions?